

1 **Investigating the fast response of precipitation intensity**  
2 **to atmospheric heating using a cloud-resolving model**

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7 **Key Points:**

- 8 • Atmospheric heating preferentially reduces weak precipitation.
- 9 • The intensity of strong precipitation events is maintained by a cancellation be-
- 10 tween thermodynamic and dynamic effects.
- 11 • Free-tropospheric heating warms the boundary layer mainly through reducing rain
- 12 re-evaporation.

**Abstract**

Coarse-resolution global climate models cannot explicitly resolve the tropical precipitation intensity distribution, and possible changes caused by forcings. We use a cloud-resolving model to study how imposed atmospheric radiative heating (such as that caused by greenhouse gases or absorbing aerosols) may alter precipitation intensity in a radiative-convective equilibrium setting. It is found that the decrease in total precipitation is realized through reducing weak events ( $< 400 \text{ mm day}^{-1}$ ). The intensity of strong precipitation events is maintained by a cancellation between thermodynamic and dynamic effects. A boundary layer energy budget analysis suggests that free-tropospheric heating raises boundary layer temperatures mainly through a reduction in rain re-evaporation. This insight leads to a predictive theory for the surface sensible and latent flux changes. The results imply that cloud process play a key role in shaping the temperature and precipitation responses to atmospheric heating.

Plain language summary: The effect of atmospheric heating on precipitation intensity is investigated using a model that can resolve moist convection. It is found that heating the entire atmosphere reduces mean precipitation and elevates water vapor concentration near the surface. The latter increases the fraction of intense rainfall. Decreased mean precipitation also weakens the re-evaporative cooling from falling rain, allowing the heating in the interior of the atmosphere to warm up near-surface air. The results show how important cloud processes are for understanding the temperature and precipitation responses to atmospheric heating.

**1 Introduction**

Greenhouse gases and absorbing aerosols warm climate by absorbing longwave and shortwave radiation, respectively. Greenhouse gases represent the strongest anthropogenic climate forcing, with top-of-the-atmosphere (TOA) values of  $2.54\text{-}3.12 \text{ W m}^{-2}$  [Myhre *et al.*, 2013]. Unlike well-mixed greenhouse gases, unevenly distributed absorbing aerosols can lead to local TOA forcing exceeding  $20 \text{ W m}^{-2}$  [e.g. Strong *et al.*, 2015]. The radiative heating gives rise to a fast (days to months) atmosphere-land response and a slow (years or longer) response that involves the ocean [e.g. Andrews and Forster, 2010]. Given the different time scales, the two responses can be treated as distinct. In fact, global climate model (GCM) simulations indicate that the fast response to atmospheric absorption acts to reduce global-mean precipitation, while the slow response has the opposite

45 effect [Andrews *et al.*, 2010; Ming *et al.*, 2010; Fläschner *et al.*, 2016]. For this reason,  
46 one can study the fast response in isolation from the slow response.

47 On fast time scales, an increase in atmospheric radiative heating must be balanced  
48 partially by a reduction in surface latent heat flux (and mean precipitation) [Andrews  
49 *et al.*, 2010; Bala *et al.*, 2010; Dinh and Fueglistaler, 2017; Richardson *et al.*, 2015]. This  
50 change in mean precipitation need not scale with, or even agree in sign, with those of  
51 precipitation extremes. For example, a study of the fast response to doubling CO<sub>2</sub> re-  
52 ported a percentage decrease in tropical cyclone frequency (-10%) that more than dou-  
53 bles that in mean precipitation (-2.3%) over the TC genesis regions [Held and Zhao, 2011].

54 The fast response of precipitation intensity to atmospheric heating has been stud-  
55 ied with GCMs. Sillmann *et al.* [2017] found that GCMs do not even agree on the sign  
56 of the annual maximum daily precipitation change caused by a quadrupling of CO<sub>2</sub>. Be-  
57 sides the lack of consensus among models, there are many well-known reasons to doubt  
58 the capability of GCMs in simulating extreme precipitation with parameterized moist  
59 convection, especially in the tropics [O’Gorman, 2015]. GCMs typically underestimate  
60 intense precipitation when compared with observations, with the biases being more se-  
61 vere for low-resolution GCMs (1° or coarser) [Stephens *et al.*, 2010; Kopparla *et al.*, 2013;  
62 Sillmann *et al.*, 2013; O’Brien *et al.*, 2016]. While the convective parameterization of  
63 a GCM can be altered to better match observations, a troubling sign is that such a mod-  
64 ification can lead to larger changes in the frequency of heavy rain than a 2-K increase  
65 in sea surface temperatures (SSTs) [Wilcox and Donner, 2007], casting in doubt the mod-  
66 els’ utility in studying extreme precipitation changes.

67 In light of GCMs’ limitations, we turn to cloud-resolving models (CRMs) on a limited-  
68 area domain, which have been shown to produce realistic simulations of heavy rain events  
69 when forced with proper boundary conditions [Fan *et al.*, 2015; Lee *et al.*, 2016; Hodzic  
70 and Duvel, 2018]. Since what is at issue here is the general characteristics of the fast re-  
71 sponse to atmospheric heating, we intentionally move away from detailed simulation of  
72 a particular region or event in favor of a setting that is more representative of the cli-  
73 mate system, namely radiative-convective equilibrium (RCE). One advantage of RCE  
74 is that both energy and moisture are conserved within the atmosphere, which need not  
75 be the case for individual events. One can think of RCE as an approximation of the trop-  
76 ical climate without large-scale mean circulation.

77 The troposphere consists of the free troposphere and boundary layer. In this pa-  
78 per, we analyze their energy balances separately to better identify the physical mech-  
79 anisms through which elevated heating affects boundary layer properties (such as tem-  
80 perature and humidity). A specific issue to be addressed is the boundary layer energet-  
81 ics. Existing works have focused on the balance among sensible heating, radiative cool-  
82 ing and entrainment of free-tropospheric air into the boundary layer [Ball, 1960; Lilly,  
83 1968]. The entrainment term is often parameterized as a fixed fraction of the surface sen-  
84 sible heat flux [0.2 or 0.25 in Betts, 1973; Tennekes, 1973; Betts and Ridgway, 1989; Betts,  
85 2000; Cronin, 2013], implying that the sensible heat flux is tightly coupled to the bound-  
86 ary layer radiative cooling. While Betts [2000] later recognized that precipitation re-evaporative  
87 cooling might contribute to the boundary layer energy balance, possible change in re-  
88 evaporation under warming is not taken into account explicitly in the analytical mod-  
89 els of climate sensitivity [Takahashi, 2009; Cronin, 2013]. This means that the bound-  
90 ary layer energy balance, and for that reason boundary layer temperature are, to first  
91 order, independent of free-tropospheric heating. This paper will test the validity of this  
92 assumption.

## 93 2 Methods

94 We use the Advanced Research Weather Research and Forecasting (WRF) model  
95 configured to run in RCE [Wang and Sobel, 2011]. Radiative transfer is reduced to a pre-  
96 scribed cooling rate in the troposphere ( $T > 207.5K$ ), and Newtonian relaxation in the  
97 stratosphere to 200K on a time scale of 5 days [Pauluis and Garner, 2006]. This highly  
98 idealized radiation scheme allows us to focus on the effects of imposed atmospheric heat-  
99 ing without complicating factors such as water vapor feedback and cloud radiative ef-  
100 fect. Sub-grid diffusion is parameterized following the YSU boundary layer scheme [Hong  
101 *et al.*, 2006] in the vertical direction, and the Smagorinsky two-dimensional scheme in  
102 the horizontal. The single-moment Purdue-Lin microphysics scheme [Lin *et al.*, 1983;  
103 Rutledge and Hobbs, 1984; Chen and Sun, 2002] contains six species: water vapor, cloud  
104 water, cloud ice, rain, snow and graupel. Surface sensible and latent heat fluxes ( $SH$  and  
105  $LH$ , respectively; both in  $W m^{-2}$ ) are calculated using the bulk aerodynamic formula  
106 with a drag coefficient of 0.001 and a constant near-surface wind speed of  $5 m s^{-1}$ :

$$SH = 0.005c_p(T_s - T_a) \quad (1)$$

$$LH = 0.005L(q_{sat} - q_a), \quad (2)$$

107 where  $c_p$  is the specific heat capacity of air ( $1004.5 \text{ J kg}^{-1} \text{ K}^{-1}$ ),  $L$  the latent heat of  
 108 vaporization ( $2.5 \times 10^6 \text{ J kg}^{-1}$ ),  $T_s$  surface temperature,  $T_a$  the lowest model level (or  
 109 near-surface) temperature,  $q_{sat}$  the saturated water vapor mixing ratio at  $T_s$ , and  $q_a$  the  
 110 lowest model level water vapor mixing ratio. Note that the density of air in the bound-  
 111 ary layer is set at  $1 \text{ kg m}^{-3}$  for the purpose of calculating surface fluxes. As  $T_s$  and  $q_{sat}$   
 112 are fixed, it is clear from Eqs. 1 and 2 that the only way to alter  $SH$  and  $LH$  is by ad-  
 113 justing near-surface boundary layer temperature and humidity ( $T_a$  and  $q_a$ ).

114 All simulations are performed on a doubly-periodic domain of  $96 \times 96$  gridpoints  
 115 with a horizontal spacing of 2 km. There are fifty vertical levels, nine of which are in the  
 116 lowest 1 km. Domain-average winds are relaxed to zero on a time scale of 2 hours to pre-  
 117 vent wind shear from developing, similar to *Tompkins and Semie* [2017]. The surface tem-  
 118 perature is set at 301.15 K, making the lower boundary conditions horizontally homoge-  
 119 nous. The two control simulations with different microphysical assumptions (to be dis-  
 120 cussed) are initialized with a warm bubble and are performed for 240 model days; the  
 121 perturbation simulations are branched off day 180 of their respective controls and last  
 122 60 model days. The last 20 days of hourly-mean outputs from each simulation are an-  
 123 alyzed. We use five consecutive, non-overlapping 20-day periods (days 220-320) for as-  
 124 sessing the noise level of any given variable. The difference between a control and a per-  
 125 turbation is considered significant if it rises above the noise level.

126 The prescribed radiative cooling rate is at the default value ( $-1.5 \text{ K day}^{-1}$ ) in the  
 127 first base case (BASE). It is reduced by half to  $-0.75 \text{ K day}^{-1}$  throughout the troposphere  
 128 in HEAT. To isolate the boundary layer response to free-tropospheric heating, we sep-  
 129 arate the uniform radiative heating into two complementary cases: halving the cooling  
 130 only above 850 hPa (A850) and below (B850). To assess the importance of rain re-evaporation  
 131 in communicating free-tropospheric heating to the boundary layer, we repeat all the sim-  
 132 ulations with a model configuration in which the rate of rain re-evaporation in the cloud  
 133 microphysics module is arbitrarily suppressed by a factor of 10. The four additional cases  
 134 are denoted by adding an asterisk to the original case names. We will refer to the two

135 groups of experiments as full and partial re-evaporation, respectively. Throughout this  
 136 paper, a response to heating is denoted with a  $\delta$ .

### 137 3 Results

#### 138 3.1 Domain-average responses

139 **Table 1.** Domain-average tropospheric radiative cooling ( $RA$ ,  $\text{W m}^{-2}$ ), surface sensible heat  
 140 flux ( $SH$ ,  $\text{W m}^{-2}$ ), surface latent heat flux ( $LH$ ,  $\text{W m}^{-2}$ ), near-surface temperature ( $T_a$ , K) and  
 141 water vapor mixing ratio ( $q_a$ ,  $10^{-3} \text{ kg kg}^{-1}$ ), precipitation ( $P$ ,  $\text{mm day}^{-1}$ ), and changes in the  
 142 perturbation cases. All changes are significant.

	$RA$	$SH$	$LH$	$T_a$	$q_a$	$P$
BASE	-145	19.5	127	297.3	14.4	4.4
$\delta$ HEAT	72	-14.7	-55.1	2.9	4.3	-1.9
$\delta$ A850	59	-11.1	-46	2.2	3.6	-1.6
$\delta$ B850	13	-4.2	-7.8	0.84	0.61	-0.27
BASE*	-145	9.4	137	299.3	13.6	4.7
$\delta$ HEAT*	72	-9.3	-61.2	1.8	4.8	-2.1
$\delta$ A850*	59	-4.7	-53.2	0.95	4.2	-1.8
$\delta$ B850*	13	-6.3	-5.7	1.3	0.45	-0.2

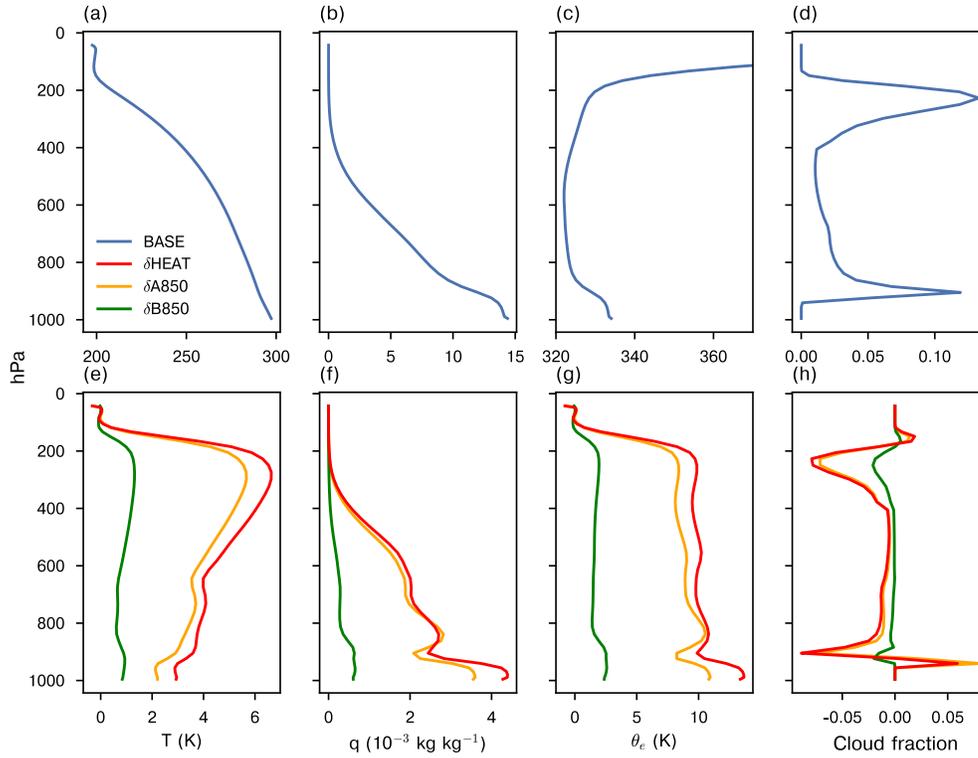
143 We begin by examining a set of key domain-average quantities and their changes  
 144 resulting from forced heating (Table 1). Relative to BASE, the tropospheric radiative  
 145 cooling (from the surface to 200 hPa) is cut by half in HEAT. The resulting net heat-  
 146 ing is balanced by reducing both surface sensible and latent heat fluxes with a ratio of  
 147  $\delta SH$  to  $\delta LH$  at 0.27, which differs significantly from the Bowen ratio in BASE (0.15),  
 148 suggesting that radiative cooling plays a role in determining the Bowen ratio. Consis-  
 149 tent with Eqs. 1 and 2, the near-surface temperature ( $T_a$ ) increases by 2.9 K, while the  
 150 near-surface water vapor mixing ratio ( $q_a$ ) increases by 30%. [The latter is greater than  
 151 what one would expect from the Clausius-Clapeyron relation and assuming constant rel-  
 152 ative humidity (RH) (20%). Indeed, the near-surface RH increases by about 10% (rel-  
 153 ative change) to make up the difference.] More quantitatively, according to Eqs. 1 and  
 154 2, the changes in  $SH$  ( $\delta SH$ ) and  $LH$  ( $\delta LH$ ) can be written as  $-0.005c_p\delta T_a$  and  $-0.005L\delta q_a$ ,

155 respectively, meaning that one can tie the near-surface temperature and humidity changes  
 156 directly to imposed heating. It is, nonetheless, unclear what determines the relative con-  
 157 tributions of sensible and latent heating, a point to which we will return in Section 3.3.  
 158 The domain-average precipitation (equivalent to latent heat flux) reduces by 43%, which  
 159 is less than the relative decrease in radiative cooling.

160 For the two differential heating cases, the column-integrated change in radiative  
 161 cooling in A850 is about 4.5 times of that in B850. This is understandable as it is ap-  
 162 proximately proportional to the pressure depth to which the perturbations are applied  
 163 [i.e.  $(850-200)/(1000-850)$ ]. The ratio is 2.6 for  $\delta T_a$ , and 5.9 for  $\delta q_a$  and  $\delta P$ , suggesting  
 164 that elevated heating is less effective at modifying surface sensible flux (near-surface tem-  
 165 perature), but more so at altering surface latent heat flux (near-surface moisture and pre-  
 166 cipitation). It is still somewhat surprising to see that the free-tropospheric heating has  
 167 a substantial warming effect on the near surface, especially given that most of the sen-  
 168 sible heating from the YSU scheme is placed in the boundary layer. This suggests that  
 169 when conjecturing a quantitative theory for the partitioning of surface sensible and la-  
 170 tent heating, one has to take into account the vertical distribution of atmospheric ra-  
 171 diative heating and the coupling between the free troposphere and boundary layer.

172 Relative to BASE, the decreased microphysical cooling in BASE\* warms the bound-  
 173 ary layer by 2 K, reducing the surface sensible heat. The tropospheric energy balance  
 174 is restored by increasing the surface latent heat flux, which is consistent with lower bound-  
 175 ary layer humidity. The response of sensible heat to the heating in HEAT\* is much smaller  
 176 ( $-9.3 \text{ W m}^{-2}$ ) than that of HEAT ( $-14.7 \text{ W m}^{-2}$ ). Note that the surface sensible heat  
 177 flux is close to zero in HEAT\*. As compared to the full re-evaporation counterparts, el-  
 178 evated heating becomes less effective in inducing boundary layer warming (1.8 K in HEAT\*  
 179 versus 2.9 K in HEAT, and 0.95 in A850\* versus 2.2 K in A850). Consequently, the re-  
 180 duction in latent heat (precipitation) is more pronounced in the partial re-evaporation  
 181 cases with free-tropospheric heating.

186 Figure 1 shows the vertical profiles of temperature ( $T$ ), water vapor mixing ratio  
 187 ( $q$ ), equivalent potential temperature ( $\theta_e$ ) and cloud fraction in BASE (top row) and their  
 188 changes in the perturbation cases (bottom row). The temperature structure in RCE fol-  
 189 lows that of a moist adiabat (Figure 1a), and to first order sets the vertical structure of  
 190 water vapor (Figure 1b) in the free troposphere.  $\theta_e$  shows a first baroclinic structure,



182 **Figure 1.** Vertical profiles of (a) temperature ( $T$ , K), (b) water vapor mixing ratio ( $q$ ,  
 183  $10^{-3} \text{ kg kg}^{-1}$ ), (c) equivalent potential temperature ( $\theta_e$ , K), (d) cloud fraction in BASE. (e-  
 184 h) Changes in (a-d) due to heating (prefixed by  $\delta$ ) in HEAT, A850, and B850. All changes rise  
 185 significantly above the noise level.

with a minimum at around 500 hPa. Under heating, the near-surface warming extends throughout the troposphere, with appreciable amplification in the middle and upper troposphere, as a consequence of moist adiabatic control (Figure 1e). In contrast, the accompanying increase in  $q$  is bottom-heavy, as in the control (Figure 1f).  $\theta_e$  increases rather uniformly throughout the troposphere (Figure 1g). As in *Wang and Sobel* [2011], a grid is defined as cloudy if the total cloud condensate (water and ice) exceeds  $0.005 \text{ g kg}^{-1}$ . Cloud fraction has two maxima in the vertical direction (Figure 1d). One can regard the lower one approximately as the lifting condensation level (LCL). It becomes lower in HEAT as the near-surface RH increases [*Romps*, 2017]. Note that the LCL remains above 950 hPa (the boundary layer top used in this paper) in all experiments. The cloud fraction in HEAT is approximately half of that in BASE (Figures 1d,h).

### 3.2 Precipitation intensity

The domain-average precipitation of the events at gridpoints where the hourly precipitation rate  $r$  exceeds a threshold value  $r_t$  (in  $\text{mm day}^{-1}$ ), is denoted as  $p(r > r_t)$  and shown in Figure 2a. By definition,  $p(r > 0)$  is the domain-average precipitation of all events ( $P$ ), which was discussed in the previous section. In BASE,  $p(r > 400)$  is about  $0.8 \text{ mm day}^{-1}$  (referred to as strong events in this work), while the rest ( $3.5 \text{ mm day}^{-1}$ ) is accounted for by weak events ( $r$  less than  $400 \text{ mm day}^{-1}$ ). Despite the substantial (43%) reduction in  $P$  in HEAT, there is almost no change ( $+0.1 \text{ mm day}^{-1}$ ) in the precipitation generated by strong events. Thus, the reduction is realized exclusively by lowering the precipitation from weak events from  $3.4 \text{ mm day}^{-1}$  in BASE to  $1.6 \text{ mm day}^{-1}$  in HEAT. This amounts to a 53% decrease.

Figure 2b plots the hourly precipitation rate against 500-hPa vertical velocity ( $w$ ) for all gridpoints in BASE and HEAT. Both quantities are strongly correlated, especially for the events with appreciable positive (upward)  $w$  (greater than  $\sim 0.1 \text{ m s}^{-1}$ ); a linear regression through the origin yields  $R = 0.67$  for BASE and HEAT. Yet, the slope ( $k$ ) for HEAT is 34% larger than for BASE, meaning that the same updraft generates considerably more precipitation in the former. This is consistent with the 30% increase in the average near-surface water vapor mixing ratio ( $q_a$ ) as discussed above. As such, the strong events in BASE can be thought of approximately as being generated by vertical motions exceeding  $2.2 \text{ m s}^{-1}$ . In comparison, the threshold stands at  $1.7 \text{ m s}^{-1}$  in

222 HEAT. One may also gather that vertical velocity is generally weaker in HEAT than in  
 223 BASE.

224 Figure 2c shows the probability of  $w$  exceeding a threshold  $w_t$  for  $w_t > 0.1 \text{ m s}^{-1}$ ,  
 225 or  $\int_{w_t}^{\infty} \mathcal{P}(w)dw$ , where  $\mathcal{P}(w)$  is the probability density function of  $w$ . Ascents are rela-  
 226 tively rare; on average only 1.0% of the grids have  $w$  larger than  $0.1 \text{ m s}^{-1}$ . The prob-  
 227 ability decreases by three orders of magnitude as  $w_t$  increases to  $5 \text{ m s}^{-1}$ . In HEAT, as-  
 228 cending motions become even less likely across the entire range of  $w_t$ , affirming the im-  
 229 pression of weaker ascents from Figure 2b.

230 To better understand the different responses of strong versus weak events, we write  
 231 the domain-average precipitation of the events with  $w$  greater than a certain positive value  
 232  $w_t$  [ $p(w > w_t)$ ,  $w_t$  in  $\text{m s}^{-1}$ ] approximately as:

$$p(w > w_t) = k \int_{w_t}^{\infty} w \mathcal{P}(w) dw. \quad (3)$$

233  $p(w > 0.1)$  is  $2.3 \text{ mm day}^{-1}$  in BASE, which accounts for slightly more than half  
 234 of the total precipitation (Figure 2d). [The remaining is associated with very weak as-  
 235 cents (less than  $0.1 \text{ m s}^{-1}$ ) and descents.]  $p(w > w_t)$  is consistently smaller in HEAT  
 236 for  $w_t$  greater than  $0.05 \text{ m s}^{-1}$ , making it easier to interpret the difference between the  
 237 two cases than in terms of  $p(r)$  (Figure 2a). To that end, one can linearly decompose the  
 238 difference [ $\delta p(w > w_t)$ ] into the thermodynamic ( $\delta k$ ) and dynamic ( $\delta \mathcal{P}$ ) terms:

$$\delta p(w > w_t) \approx \delta k \int_{w_t}^{\infty} w \mathcal{P}(w) dw + k \int_{w_t}^{\infty} w \delta \mathcal{P}(w) dw. \quad (4)$$

239 Figure 2e indicates that although this decomposition underestimates the difference  
 240 between BASE and HEAT, it does capture some important characteristics of the sim-  
 241 ulations (e.g.  $\delta p(w > w_t)$  generally decreases as  $w_t$  increases). While the thermodynamic  
 242 effect owing to higher near-surface water vapor mixing ratio acts to enhance precipita-  
 243 tion, the dynamic effect in the form of weaker ascents tends to lower precipitation. As  
 244 the dynamic effect outweighs the thermodynamic effect, the net result is a reduction of  
 245 precipitation at a given  $w_t$ . To address the question why the precipitation from strong  
 246 events [ $p(r > 400)$ ] is similar between BASE and HEAT, one also needs to consider that  
 247 it requires less vigorous ascents to produce these events (defined in terms of  $r$ ) in HEAT

248 than in BASE. As noted before, the threshold  $w_t$  is  $1.7 \text{ m s}^{-1}$  in HEAT, as opposed to  
 249  $2.2 \text{ m s}^{-1}$  in HEAT. This factor makes up the net reduction of precipitation after the  
 250 cancellation of the thermodynamic and dynamic effects, resulting in little change in terms  
 251 of  $p(r > 400)$ .

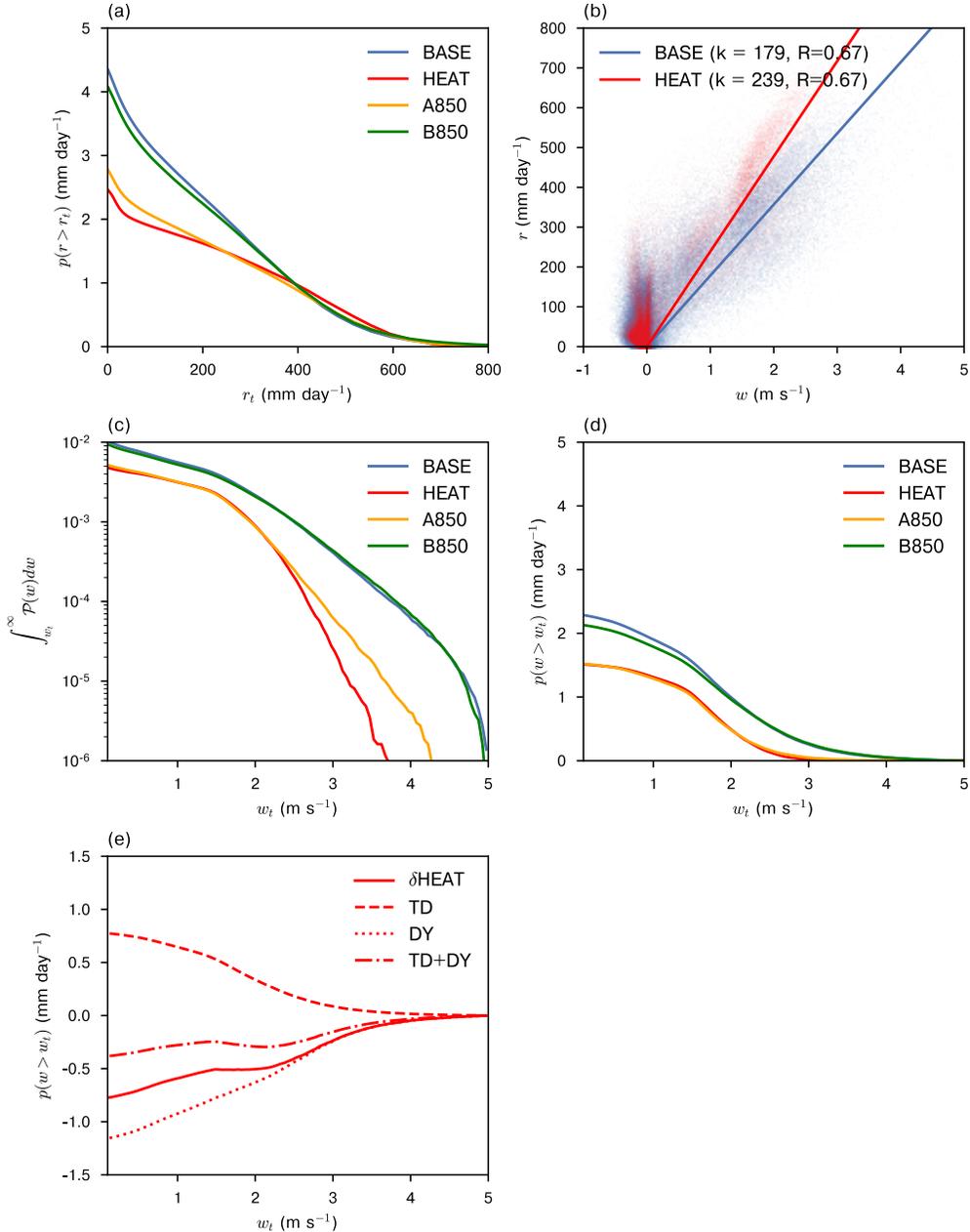
### 260 **3.3 Boundary layer energy balance**

261 Surface sensible heat ( $SH$ ) is the main energy source for the boundary layer in BASE  
 262 (Figure 3a). Additional heating is realized through the exchange of sensible heat with  
 263 the free troposphere, either explicitly resolved or parameterized at the sub-grid scale ( $EX$ ).  
 264 The sink terms are radiative cooling ( $RA_b$ ) and re-evaporative cooling ( $RE$ ) in the bound-  
 265 ary layer. The latter takes place as rain falls through the unsaturated boundary layer  
 266 and is thus microphysical in nature. Somewhat surprisingly, the magnitude of re-evaporative  
 267 cooling is larger than that of radiative cooling, which is often presumed to be the dom-  
 268 inant sink term.

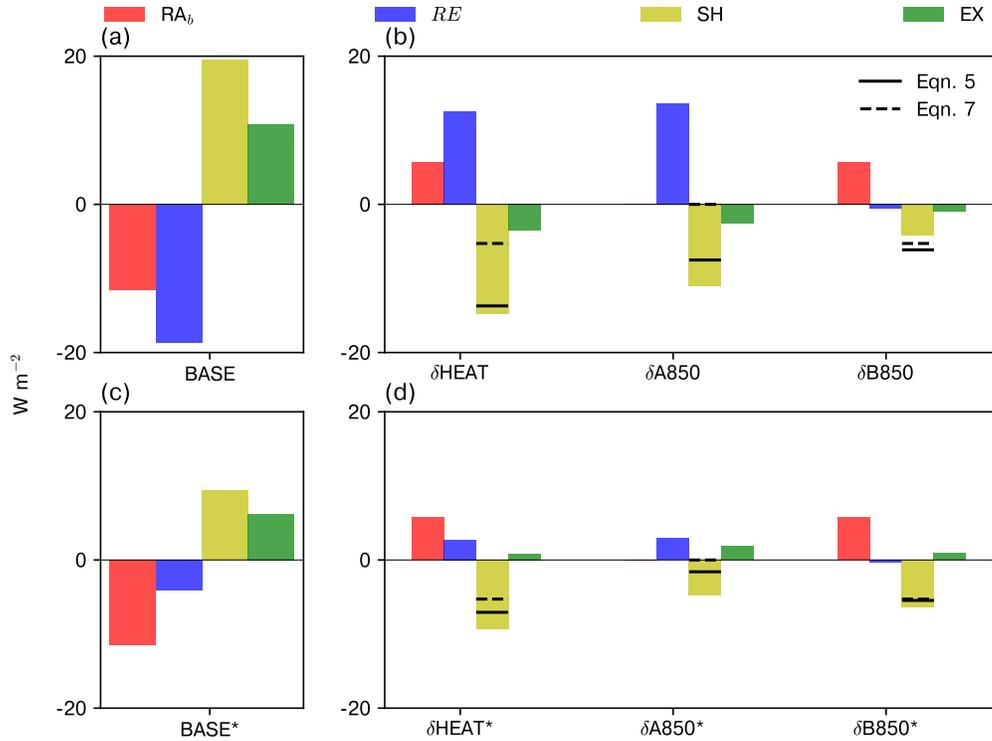
274 Figure 3b summarizes how the individual terms vary in the perturbation cases. Al-  
 275 though imposed radiative heating is clearly present in HEAT, the main balance is be-  
 276 tween  $SH$  and  $RE$ , both of which decrease substantially in magnitude. As A850 and B850  
 277 add up roughly to HEAT, one can see that the boundary layer radiative heating is bal-  
 278 anced almost entirely by lowering  $SH$ , as is the case in B850. The large reduction in  $RE$   
 279 seen in HEAT can be attributed to the radiative heating above 850 hPa, and amounts  
 280 to a warming effect on the boundary layer. This is consistent with lower  $SH$  and higher  
 281 near-surface temperature (Table 1). The changes in  $EX$  are much smaller than those  
 282 in  $SH$  in all cases.

283 One can define precipitation efficiency ( $\epsilon$ ) as the ratio of precipitation ( $P$ ) over column-  
 284 integrated condensation ( $C$ ) [Zhao, 2014], with a value of 0.33 in BASE. Re-evaporation,  
 285 which is equal to the difference between  $C$  and  $P$  (i.e.  $C - P$ ), can be written as  $P(1 -$   
 286  $\epsilon)/\epsilon$ . As  $\epsilon$  is little changed across the cases (within 0.01), the fractional changes in column-  
 287 integrated re-evaporation and precipitation should be similar to each other. This rela-  
 288 tion also holds approximately for boundary layer re-evaporation (i.e.  $\delta RE/RE = \delta P/P$ ),  
 289 which decreases by 64% in BASE in comparison with a 43% reduction of precipitation.

290 The partial re-evaporation simulations allow us to further assess the importance  
 291 of re-evaporation. Despite having the same boundary layer radiative cooling as BASE,



252 **Figure 2.** (a) The domain-average precipitation ( $p(r > r_t)$ , mm day<sup>-1</sup>) of the events whose  
 253 hourly precipitation rates exceed  $r_t$  (mm day<sup>-1</sup>) in the full re-evaporation experiments. (b) The  
 254 scatter plot of  $r$  (mm day<sup>-1</sup>) against 500-hPa vertical velocity ( $w$ , m s<sup>-1</sup>) for BASE and HEAT.  
 255 The solid lines are the best-fit lines with zero-intercept for  $w > 0.1$  m s<sup>-1</sup>. (c) The probability of  
 256  $w$  exceeding a threshold  $w_t$  (m s<sup>-1</sup>), or  $\int_{w_t}^{\infty} \mathcal{P}(w) dw$ , for  $w_t > 0.1$ . (d) The domain-average pre-  
 257 cipitation ( $p(w > w_t)$ , mm day<sup>-1</sup>) of the events where  $w$  exceeds  $w_t$ , estimated with Equation 3.  
 258 (e) The difference in  $p(w > w_t)$  between BASE and HEAT, and its thermodynamic and dynamic  
 259 components and their sum, estimated with Equation 4.



269 **Figure 3.** (a) The individual terms in the boundary layer energy balance ( $W m^{-2}$ ) in BASE:  
 270 surface sensible heating ( $SH$ ), radiative cooling ( $RA_b$ ), re- evaporative cooling ( $RE$ ) and the ex-  
 271 change of sensible heat with the free troposphere ( $EX$ ). (b) Changes in HEAT, A850 and B850.  
 272 (c,d) Same as (a,b), but for the partial re- evaporation cases. The solid and dashed lines denote  
 273 the change in  $SH$  calculated from Equations 5 and 7, respectively.

292 the magnitudes of the surface sensible heating and the exchange term are much reduced  
 293 in BASE\*, presumably due to the suppressed re- evaporative cooling (Figure 3c). The  
 294 response to free-tropospheric heating is also muted considerably in A850\*; the result-  
 295 ing reduction in  $SH$  is less than half of that in A850. The same is true for near-surface  
 296 temperature (Table 1). This reaffirms the importance of re- evaporative cooling in com-  
 297 municating the effect of free-tropospheric heating to the boundary layer and surface.

#### 298 4 Discussion and summary

299 It is clear from the above results that the vertical distribution of radiative heat-  
 300 ing is key to determining the relative roles of surface sensible and latent heat adjustments  
 301 in re-establishing the tropospheric energy balance. In particular, re- evaporative cooling  
 302 is the main process through which the effect of free-tropospheric heating can be felt by  
 303 the boundary layer and surface. Thus, re- evaporation has to be considered explicitly in  
 304 any attempt to develop a quantitative theory of the surface turbulent flux response to  
 305 atmospheric heating.

306 If one assumes that the free-tropospheric energy balance can be approximated as  
 307 radiative cooling balancing out latent heating, it follows that the fractional change of pre-  
 308 cipitation is equal to that of the free-tropospheric radiative cooling ( $\delta P/P = \delta RA_f/RA_f$ ).  
 309 As discussed before, the fractional change of the boundary layer re- evaporative cooling  
 310 is approximately equal to that of precipitation. Thus,  $\delta RE$  can be written as  $\alpha \delta RA_f$ ,  
 311 where  $\alpha$  is the ratio of  $RE$  to  $RA_f$  in the base case. If the exchange term does not vary  
 312 appreciably with imposed heating, the boundary layer energy balance leads to the fol-  
 313 lowing expression of the surface sensible heat flux change:

$$\delta SH = -\delta RA_b - \alpha \delta RA_f. \quad (5)$$

314 Furthermore, its latent heat counterpart can be derived from the tropospheric en-  
 315 ergy balance:

$$\delta LH = (\alpha - 1) \delta RA_f. \quad (6)$$

316 This constitutes a predictive theory of  $\delta SH$  and  $\delta LH$  in response to  $\delta RA_b$  and  $\delta RA_f$   
 317 as  $\alpha$  (0.13 in BASE) depends only on values in BASE. The predicted  $\delta SH$  is in good agree-

318 ment with the simulations (Figure 3). According to this theory, free-tropospheric heat-  
 319 ing reduces latent heating more than sensible heating as long as  $\alpha$  is smaller than 0.5.  
 320 Also, boundary layer heating decreases sensible heating only.

321 The approximation used in *Takahashi* [2009] and *Cronin* [2013] can be viewed as  
 322 a special case of Equation 5 with  $\alpha = 0$ :

$$\delta SH = -\delta RA_b. \quad (7)$$

323 The partial re-evaporation experiments allow us to test the theory for a small value  
 324 of  $\alpha$  (0.02 in BASE\*) that approaches this special case. Indeed, the predictions from Equa-  
 325 tions 5 and Equation 7 are much closer than for the full experiments. In other words,  
 326 the  $\alpha\delta RA_f$  term in Equation 5 greatly improves the accuracy of the predicted  $\delta SH$  by  
 327 incorporating the effect of re-evaporation in coupling the boundary layer and the free-  
 328 troposphere.

329 In summary, imposed radiative warming reduces domain-average precipitation (evap-  
 330 oration) by increasing boundary layer water vapor, a thermodynamic effect that tends  
 331 to enhance precipitation rate at a given vertical velocity. This effect opposes the weak-  
 332 ening of ascents (a dynamic effect), resulting in no significant change in the precipita-  
 333 tion from strong events. The decrease in domain-average precipitation is realized entirely  
 334 through weak events. A key finding is that free-tropospheric radiative heating affects the  
 335 boundary layer and surface properties primarily by weakening the re-evaporative cool-  
 336 ing. This insight leads to a predictive theory of the surface latent and sensible heat flux  
 337 changes caused by radiative heating.

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